



INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification ⁶ : A61B 3/14, 3/10, 3/00</p>	<p>A1</p>	<p>(11) International Publication Number: WO 97/30627</p> <p>(43) International Publication Date: 28 August 1997 (28.08.97)</p>
<p>(21) International Application Number: PCT/IL97/00065</p> <p>(22) International Filing Date: 20 February 1997 (20.02.97)</p> <p>(30) Priority Data: 117241 23 February 1996 (23.02.96) IL</p> <p>(71) Applicant (for all designated States except US): TALIA TECHNOLOGY LTD. (IL/IL); P.O. Box 3780, 90805 Mevaseret Zion (IL).</p> <p>(72) Inventors; and (73) Inventors/Applicants (for US only): KARPOL, Avner (IL/IL); 4G Tepper Street, 70400 Nes Ziona (IL). ZEIMER, Ran (IL/US); Johns Hopkins Hospital, Woods Research Building, Room 355, 600 North Wolfe, Baltimore, MD 21287-9278 (US).</p> <p>(74) Agent: NOAM, Meir; P.O. Box 32081, 91320 Jerusalem (IL).</p>		<p>(81) Designated States: AL, AM, AT, AU, AZ, BB, BG, BR, BY, CA, CH, CN, CZ, DE, DK, EE, ES, FI, GB, GE, HU, IS, JP, KE, KG, KP, KR, KZ, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, TJ, TM, TR, TT, UA, UG, US, UZ, VN, ARIPO patent (KE, LS, MW, SD, SZ, UG), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG).</p> <p>Published With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</p>
<p>(54) Title: A THREE DIMENSIONAL IMAGING APPARATUS AND A METHOD FOR USE THEREOF</p> <div data-bbox="310 723 735 1065"> </div> <p>(57) Abstract</p> <p>A three dimensional imaging scanning apparatus for determining the retinal thickness of an eye (13) and the structure non-invasive analysis comprising an optical unit (19) including a light source (1a), a shaping and focussing optics (8, 9), a beam deflector (11) for scanning the light beam emitted from the light source on the retinal tissues (13b) and detector (16) for detecting the reflected light beam from the retinal tissues; a computer (20) for processing the representations and composite imagery which display on a display means (21).</p>		

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AM	Armenia	GB	United Kingdom	MW	Malawi
AT	Austria	GE	Georgia	MX	Mexico
AU	Australia	GN	Guinea	NE	Niger
BB	Barbados	GR	Greece	NL	Netherlands
BE	Belgium	HU	Hungary	NO	Norway
BF	Burkina Faso	IE	Ireland	NZ	New Zealand
BG	Bulgaria	IT	Italy	PL	Poland
BJ	Benin	JP	Japan	PT	Portugal
BR	Brazil	KE	Kenya	RO	Romania
BY	Belarus	KG	Kyrgyzstan	RU	Russian Federation
CA	Canada	KP	Democratic People's Republic of Korea	SD	Sudan
CF	Central African Republic	KR	Republic of Korea	SE	Sweden
CG	Congo	KZ	Kazakhstan	SG	Singapore
CH	Switzerland	LJ	Liechtenstein	SI	Slovenia
CI	Côte d'Ivoire	LK	Sri Lanka	SK	Slovakia
CM	Cameroon	LR	Liberia	SN	Senegal
CN	China	LT	Lithuania	SZ	Swaziland
CS	Czechoslovakia	LU	Luxembourg	TD	Chad
CZ	Czech Republic	LV	Latvia	TG	Togo
DE	Germany	MC	Monaco	TJ	Tajikistan
DK	Denmark	MD	Republic of Moldova	TT	Trinidad and Tobago
EE	Estonia	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	UG	Uganda
FI	Finland	MN	Mongolia	US	United States of America
FR	France	MR	Mauritania	UZ	Uzbekistan
GA	Gabon			VN	Viet Nam

A THREE DIMENSIONAL IMAGING APPARATUS AND A METHOD FOR USE THEREOF

FIELD OF THE INVENTION

The present invention generally relates to a three dimensional imaging apparatus and a method for use thereof. More specifically the present invention relates to a retinal tissue components size and thickness analyzer apparatus. The said invention furthermore relates to a non invasive measurement method for measuring retinal thickness imaging and for visualizing retinal cross sections by using said apparatus. The apparatus according to the said invention incorporates laser and conventional optics with computerizes signal analysis in order to measure pathological indications in the eye and in order to identify normal ocular physiology. This allows for improved diagnosis for various ophthalmic diseases such as diabetic retinopathy and glaucoma, and also for improved monitoring of therapeutic effects.

BACKGROUND OF THE INVENTION

The two main causes of blindness in the western world are diabetic retinopathy and glaucoma.

One of the most important pathologies of diabetic retinopathy is macular edema. Over a lifetime, about 30% of the people with diabetes will develop macular edema. Nonproliferative diabetic retinopathy with Clinically Significant Macular Edema (CSME) includes either (a) thickening of the retina at or within 500 microns of the center of the macula or (b) hard exudates at or within 500 microns of the center of the macula if associated with thickening of the adjacent retina (not residual hard

exudates remaining after the disappearance of retinal thickening) or (c) a zone or zones of retinal thickening 1 disk area or larger, any part of which is within 1 disk diameter of the center of the macula. Patients with CSME should be considered for treatment.

The assessment of retinal thickening by slit lamp biomicroscopy and/or stereo fundus photography is often difficult, not accurate, and of questional reliability. Moreover, the current methods typically necessitate a time consuming involvement of a highly skilled observer. Currently there is no commercially available method, capable of detecting and mapping quantitatively retinal thickening. Thus accurate assessment of CSME in patients remains subjective even though the clinical criteria of CSME are quantitative. The present invention enables the necessary objective quantitative measurements to be performed.

Loss of vision from glaucoma is largely preventable through early diagnosis and therapy. While the level of Intra Ocular Pressure (IOP) is strongly correlated with the risk of glaucoma optic nerve damage, a substantial proportion of patients with glaucoma (one sixth or more) have not had demonstratable or repeated elevations of IOP above 21 mm Hg. Conversely, many individuals with IOP repeatedly above 21 mm Hg do not have, and may never develop, optic nerve damage during their lifetime.

Screening procedures for identifying patients at significant risk for glaucomatous visual field loss are most effective when IOP measurements are combined with an assessment of the optic nerve and a review of other potential ocular and systemic risk factors. This approach is already part of the "Comprehensive Adult Eye Examination", which may constitute the single most important screening/diagnostic setting to identify patients

at risk and a subset of those at particularly "high risk" for glaucoma.

Visible structural alterations of the optic nerve or nerve fiber layer frequently occur before visual defects can be measured, even with the most sensitive current techniques. While measures of both structure and function are important to detect early glaucomatous damage, careful and repeated examination of the optic nerve and nerve fiber layer may provide the earliest signs of damage by demonstrating progressive damage before definitive visual field abnormalities appear. The present invention allows an objective method for nerve fiber layer damage assessment.

SUMMARY OF THE INVENTION

The present invention relates to a three dimensional imaging scanning apparatus for retinal thickness and structure non-invasive analysis. The present invention also relates to a method for the use of said apparatus.

The apparatus according to the present invention is comprised of at least one optical path having:

(A) A high brightness light source or a laser which provides a beam for illuminating a selected portion of the retinal tissue.

(B) A means for simultaneous focusing said beam going to the retina and returning from the retina wherein the said focusing means are common for both the beam going to and coming from the retina.

(C) An optical beam deflector which is common for both the beam going to and coming from the retina.

(D) An aperture for defining the angle between the beam going to the retina and returning from the retina.

(E) A detection means for detection of the returned beams and determination of the retinal thickness.

(F) A camera for imagining the pupil/iris is preferably added, which enables accurate longitudinal and perpendicular positioning of the beam from (A) on the pupil.

(G) A fundus camera for imagining the whole Fundus preferably added, which enables accurate longitudinal and perpendicular positioning of the beam from (A) on the retina.

The present invention further relates to a method for imaging the eye and its components using the apparatus according to the present invention, comprising;

(a) simultaneously using three optical paths for scanning the retina using a common optical beam deflector or deflectors to illuminate a predetermined zone of the retina and to acquire an image of said zone, while vibrating said beam deflector during said illumination/acquisition time, and said vibrations improve the image quality; imaging the whole Fundus; and imaging of the pupil/iris;

(b) subsequently spatially integrating one or more of said imagings into an eye model.

DETAILED DESCRIPTION OF THE INVENTION

The retinal thickness analyzer apparatus according to the present invention operates basically on the principle of slit lamp biomicroscopy. A narrow slit of light (laser light as a preferred embodiment) is projected onto the retina. The light scattered back from the retina is viewed by an electronic camera at an angle relative to the angle of the incident light. This provides a quantitative measurement of the retinal thickness cross-section topography for the specific retinal area selected and optical sectioning of the retina.

During one measurement the slit of light is scanned over a number of positions on the retina so that the resulting image represents a number of cross-sections of the retina covering a square area of for example 2x2 mm. It is possible for example that nine adjacent squares are scanned to provide coverage of about 6x6 mm (20"x20") around the fovea, disk, or any other interesting zone. Likewise numerous contiguous or dispersed areas of the retina can be measured and the resulting three dimensional representations of the whole scanned area can be represented to enable a clinical and scientific evaluation. The retinal examination with the retinal thickness analyzer apparatus according to the present invention is performed in a manner similar to Fundus photography. After the eye is dilated and the patient is seated in the headrest of the apparatus, the apparatus is positioned along the optic axis of the eye at the correct working distance with reference to the iris display which shows a high magnification image of the iris of the examined eye. After alignment an image of the stationary slit on the retina is displayed, the focus adjustment knob is used to focus this image.

After focusing the scan is initiated. The display shows a set of slit images obtained at the positions scanned before. A thickness map, that can be displayed and/or stored for future reference, is generated by computer processing of the scanned slit images, within a short time. Different regions on the retina are scanned by translating the subjects fixation point. This is accomplished with the internal fixation target which is projected on the retina of the subjects eye. An external fixation light is also available for patients who have difficulty fixating on the internal target.

The present invention relates to a three dimensional imaging scanning apparatus for retinal thickness and structure non-invasive analysis. The present invention also relates to a method for the use of said apparatus.

The apparatus according to the present invention is comprised of at least one optical path having:

(A) A high brightness light source or a laser which provides a beam for illuminating a selected portion of the retinal tissue.

(B) A means for simultaneous focusing said beam going to the retina and returning from the retina wherein the said focusing means are common for both the beam going to and coming from the retina.

(C) An optical beam deflector which is common for both the beam going to and coming from the retina.

(D) An aperture for defining the angle between the beam going to the retina and returning from the retina.

(E) A detection means for detection of the returned beams and determination of the retinal thickness.

In the preferred embodiment of the present invention optical paths and cameras are included for imaging both the whole Fundus and the pupil/iris.

These five apparatus elements allow the retinal thickness and structure non-invasive measurement to be performed. For purposes of accomplishing said measurement for a specific region of the retina, whole fundus imaging and imaging of the pupil/iris is used. The fundus imaging is specifically employed to provide physiological spatial orientation when selecting and also when subsequently comparing specific regions of the retina. The pupil/iris imaging is specifically employed to allow selection of a point like region of the pupil plane, having acceptable or advantageous optical properties. This point like region

serves as the window through which the actual retinal measurement is accomplished.

The present invention will be further described in detail by Figures 1-4. These figures are solely intended to illustrate the preferred embodiment of the invention and are not intended to limit the scope of the invention in any manner.

Figure 1 illustrates a block diagram of the device according to the present invention.

Figure 2 represents a block diagram of the optical unit of the device.

Figure 3 is a schematic illustration of the major electro-optical components of the present invention.

Figure 4 represents a schematic graph of beam position in the eye versus time.

Detailed Description of the Figures

Figure 1 illustrates a block diagram of the device according to the present invention. An optical unit (19) illuminates the eye (13) including the retinal tissue contained therein. The light returns from the eye to the optical unit where said light is measured by optical sensors. The electronic signal from the optical sensors is transmitted to a computer processor (20). The computer processor displays representations and composite imagery on a display monitor (21).

Figure 2 represents a block diagram of the optical unit of the device. In the optical unit [(19) in Figure 1] of the apparatus according to the present invention, light

originating from a light source (15a) (halogen lamp) passes through a condenser lens (15d) (collimator lens), passes through a target pattern (15b) where the target pattern is imposed filter-wise onto the light. The light thus filtered passes through or under a common beam deflector (11). The light then proceeds through a objective lens (12) and onto the eye (13) and its inner tissues. Some portion of this incident light is reflected back through the same objective lens (12), through or under the beam deflector (11) and to a fundus mirror (14) where the returning reflective light is sensed by a fundus camera (7).

A second optical path in the optical unit begins with light originating from an eye illuminating light source (22) (for example an iris illuminating LED) which directly illuminates the eye (13). Light reflected back from the iris (13c) passes through the objective lens (12) and is reflected by a beam splitter (18) (e.g. dichroic mirror for near infra-red) where the returning reflected light is sensed by an iris camera (17) (e.g. sensitive to near infra-red).

A third optical path in the optical unit begins with a light beam originating from a laser (1a) and passing through shaping and focussing optics (8) (9). The light beam so attenuated and modified is then reflected through an aperture (10) and through the common beam deflector (11) where organized time dependent angular variations are imposed onto the light beam. The beam then passes through the common objective lens (12) and onto the eye (13) and its retinal tissues (13b). Returning scattered light from the retinal tissues passes back through the objective lens, beam deflector, lenses (9) (8), aperture (10), and is detected by the laser camera (16) (CCD).

Figure 3 represents a profile schematic illustration of the major electro-optical components of the present invention apparatus. A coherent monochromatic laser beam (1) (or a very bright light source) in green (or yellow or orange) e.g. 543 nm originated from a HeNe laser (1a) (also may be other types of lasers or a bright diode or a high brightness lamp) is reflected by a mirror (2a) and passing through an attenuator (3) (at least one attenuator). The attenuator may be mounted on a solenoid (so that changes in the solenoid's position allow for changes in the intensity exiting from the attenuator). Thus the light exiting from the attenuator is in compliance with the FDA (Food and Drug Administration - USA) standards and requirements, for limiting the intensity of the light exposure to the retina. The attenuated light also allows for compensation in eyes of different scattering coefficients.

The laser beam traverses a negative lens (4) (may also be a positive lens) which is the first part of the beam expander and which widens the beam. Thereafter the widened beam is reflected by a mirror (2b), passes through a cylindrical lens (5) changing the beam profile so that the subsequent profile of the beam at the retina is slit shaped and not dot shaped. The lens position and focal length is such that the beam cross section is small enough to traverse the eye's pupil. The laser beam is then reflected by a mirror (2c) and traverses through one side of a positive lens (8) which is the second lens of the laser beam expander, and this positive lens (8) is the complimentary corrective step to the negative lens (4). This composite beam expander insures appropriate width on the fundus. It should also be noted that by "one side" of lens (8) we mean to a position which is off axis of the lens. In another embodiment of the present invention this off-of-center optic geometry may not be used.

From this lens (8) goes out a parallel beam to focus lens (9). This lens, the focus lens, is focusing the beam to a small dot in a focal distance between lenses (9) and (12) and subsequently the beam passes through the focal plane of objective lens (12). Movement along the optic axis of focus lens (9) enables compensation for refractive variations in the eye to be examined. The laser beam then is reflected by the common beam deflector (11), or by any other optical scanner known in the art such as holographic or acoustoptic. This beam deflector is a small thin mirror with a small scanning angle and a fast response time. The common beam deflector (11) is near the location of the image of the pupil (13a) of the patient. Because the laser beam is falling on the mirror at a point which is not perturbed by minor changes of the mirror's angle, this beam will fall on a predetermined point near the pupil that likewise will not move during the scanning. Lenses (4) (5) (8) (9) and (12) constitute a beam shaping unit for insuring appropriate width and height of the beam on the fundus.

It is possible to insert a holographic or electro-optic element near the location of the image of the pupil (13a) of the patient. This element will split the laser beam into multiple beams, so that on the retina more than one laser line will be simultaneously projected.

The laser beam from the common beam deflector (11) goes to the objective lens (12) from which it goes out in parallel beam (when working with emmetropic eye). This parallel beam will rotate to the sides during the rotation of the common beam deflector (11). This rotation of the beam will cause the laser line on the retina to move. The beam deflector mirror will move to enable the laser slit profile to move 2 mm on the retina (13b).

Part of the scattered light from the retinal layers returns through the iris (13c) and the objective lens (12) to the common beam deflector (11). This light passes through an aperture (10) located near the plane of the pupil image so as to define the area on the pupil of collected scattered light. The distance between the laser beam and the aperture (10) at the aperture area defines the distance at the area of the pupil between the incident beam and the measured scattered beams ultimately going to the CCD camera (16).

The reflected beam is passing through a focus lens (9). In the place where there is a focus adjustment for the laser beam, the scattered beam from the eye makes a parallel beam to the incident beam between lens (8) and (9). The focus adjustment is necessary in order to compensate refractive error in the examined eye. The beam returning through lens (8) becomes focused into a sharp image in a focal plane.

There is a CCD camera (16) located in said focal plane. This CCD camera receives the scattered light returning from the retinal tissue. At the entrance to the CCD camera there is a filter (6) which transfers the scattered laser light but blocks both direct and scattered lamp light.

The lenses (8) and (9), the aperture (10), and the mirror (2c) are near the common beam deflector (11). In this way it is guaranteed that there is no overlapping between the incident beam to the eye and the scattered laser beams returning from the eye and coming to the CCD camera.

The lenses (8) and (9), the common beam deflector (11), and the objective lens (12) are common optical elements. The incident laser beam passes through these elements or is reflected by them prior to interaction with the eye components, and also subsequent to said interactions. The scattered laser light returns through these same elements before hitting the CCD camera. Because these optical

elements are common to both the incident and the scattered light, any small movement of one of these optical elements will not cause the apparatus to diverge from correct adjustment. This is because the error introduced into the incident beam by one of the elements is by definition exactly compensated for by the same element when the scattered return beams pass through or are reflected by said element.

Because the focussing lenses are common optical elements, only one focus element adjustment is necessary since this single adjustment corrects both the incident focus and the scattered return focus. Were this not the case, it would be necessary to adjust the incident optical element and the scattered return optical element.

Because the beam deflector is one of the abovementioned common optical elements (both for the incident and reflected laser beams), the retinal slit image will not move on the CCD camera during scanning. This enables using a camera of small dimensions in the scan axis, even when a very wide area is scanned on the retina.

We can also locate the camera so that the laser's narrow and long slit image is parallel to the horizontal pixels of the camera, effectively lowering the needed bandwidth and number of pixels of the camera in this dimension without losing retinal thickness details.

We can move the aperture (10) and by this movement we are changing the angle between two beams - the incident beams to the retina and the scattered beams from the retina. This also changes the distance between the laser beam incident on the cornea, and detected scattered beam from the retina through it thus enabling a change in the zone used in the pupil. Because the incident and scattered beams are close one to the other, and even given the small aperture opening of the dilated pupil, the best zone in the cornea and the

dilated pupil can be selected for use. Thus there exists the possibility to shift the location on the cornea through which the incident and scattered beams will traverse, thus allowing the avoidance of optical or physical defects in the cornea.

The apparatus according to the present invention has also a halogen lamp (15a). The light from the halogen lamp (15a) goes through a colimator lens (15d) and is then projected to the objective lens (12). Near the colimator lens (15d) there is a target pattern (15b) inscribed with the image of numbers one through nine. In the light path of the halogen lamp there is a filter (15c) (green, yellow, orange) for selection of the most appropriate light for Fundus photography. This halogen lamp light passes near the common beam deflector (11) in the incident direction and is collected and directed to a Fundus camera (7) by a fundus mirror (14). Near the beam deflector an aperture is located in the way of the scattered beam so that there is no overlap between the incident and the scattered beams. This eliminates cross talk between the beams in order to obtain a good contrast in the fundus image.

Near the objective lens (12) there is a light source (22) (iris illuminating LED) which illuminates the eye, and a dichroic mirror (18) (beam splitter) (which reflects a light wavelength that is not used by the laser camera nor by the Fundus camera (e.g. Near Infra-red light), and this wavelength is used in the iris imaging). This mirror reflects light from the cornea to a camera (17) (iris camera) for imaging of the pupil and the iris.

The apparatus according to the present invention has three electronic cameras: a CCD camera (16) for imaging the retinal thickness, a fundus camera (7) for imaging the whole Fundus, and a third camera (17) for imaging the pupil/iris.

The video from the three cameras is trasfered to a computer by a frame grabber card, processed, and displayed on a screen or screens. Also on the same screen or another screen is at least one text area, the content of which is determined through an operator interface.

Prior to initiating the retinal thickness measurements, the operator sees the tripartite composite image on the screen, except the the laser beam scan area is outlined. This allows the operator to select (a) the desired area of the fundus for the subsequent thickness measurement as defined by the outline, (b) the optimal settings for acquiring the area in the cornea through which said measurement will be performed as is evident from the response of the sample laser slit pattern quality, (c) optimal focus of the slit image.

Because the retinal thickness measurement image is slit shaped for each measurement taken and because for each such measurement taken during a given scan series said slit pattern is central to the CCD derived image, computer processing is required to integrate the beam deflector orientation with the corresponding image so that the image series can be properly organized with respect to corresponding locations on the retina. Said organization for a single scan series is a collection of parallel slit images, For example if we scan a 2 mm section of the retina then the beam deflector iteratively measures and jumps 200µ until it completes the 2 mm section and this results in a parallel series of 10 slit shaped thickness profiles.

The image of the laser slit scattered from the retina is composed of (a) scattering signal from the two layers that are at the edges of the retina (Pigment Epithelium - Choroid layer and Inner limiting membrane), and (b) a signal from the internal volume between those layers. Sometimes (c) a signal is seen from other layers and material near the retina, for example the membranes.

The image processing algorithm calculates the distance between the two peak signals that represent the two sides of the retina. This calculation is performed on the slit images every given 200 μ m distance along the length of the laser slit.

After image processing, various representation formats can be selected to allow for the best use of the mapping of thickness data. For example: (a) iso-thickness countour lines can be drawn, (b) a false coloration scale can be imposed in a thickness relevant fashion, (c) the data can be graphed onto various coordinate systems so as to allow best visualization of potential causal correlations, (d) comparative transformations with previous imagery for the same area for the same patient or according to demographic, genetic, physiological, or other factors can be represented, (e) numeric values for patient treatment evaluation and for comparison with previous or future results.

The apparatus according to the present invention can be adjusted to scan different locations of the retinal tissue. This is accomplished by directing the patient to fixate on one of the numericly labled locations on a projected target image (15b). Alternately the patient can be directed to fixate with the other eye on a small light source which the operator can move, and this causes the eye to be measured to fixate in a parallel-like fashion.

The area of the retina to be measured appears on the apparatus's computer monitor as a square outline superimposed on the imagery from the Fundus camera. The basic square outline in the preferred embodiment of the present invention corresponds to a region of 2 mm x 2 mm on the retinal tissue. Subsequently to the scanning measurement, the thickness profile data is saved in association with the Fundus imagery so that in subsequent representations of the

measurements, multiple measured areas can be shown simultaneously. The operator or the computer can select at least one "landmark" on the fundus to allow fundus images to be aligned. A "landmark" can be an easily identifiable blood vessel bifurcation or a morphologic anomaly. This use of landmarking helps guarantee that both the tiling of contiguous squares and their relation to other dispersed square regions will be represented with the proper spatial relationship.

When either a light source with a long coherence length is used or when the area being measured scatters light in a non-uniform manner, the subsequent measurement of the cross sections of the slit shaped beam as scattered from the retinal tissue is noisy. The resultant picture is characterized by rapid changes in signal intensity, originating from macro-scopic structure in the area. The effect of this noise in the region of any given cross section is to cause the otherwise clear bi-modal intensity distribution corresponding to the thickness of the retinal tissue to be a multi-modal intensity distribution, which leaves the thickness measurement interpretation of the data in an ambiguous state.

In a preferred embodiment of the present invention this noise problem is eliminated through a signal averaging procedure called "speckle removal". The speckle removal technique is a type of neighborhood averaging wherein the scanned area is moved slightly during the actual measurement. This may slightly reduce the lateral resolution with regard to positioning on the retina but greatly reduces the thickness measurement ambiguity problem. This technique can be used because the CCD camera receives scattered return light from the retina through the same beam deflector as the emitted light to the retina, thus guaranteeing that the image on the CCD stays sharp, since the image of the laser line that moves on the retina

does not move and smear the image on the CCD while the small amplitude scan is performed.

For example, we take an image within 0.02 sec of the scattered laser line on the retina. The laser line width on the retina is 20μ . Speckles and retinal non-uniformity size is 30μ . During this time (0.02 sec) we move the laser beam on the retina 75μ across the beam length. The scattered light is composed of the spatial average signal for the whole zone over which the laser beam moved during the imaging time. In this image too, speckles and retinal non-uniformities are averaged and therefore their noise is reduced. The image on the imaging device is not smeared due to the movement of the laser beam since it uses the same beam deflector mirror and optical path.

Super-imposed movements (vibrations) of predetermined amplitude and shape, and are super-imposed onto the normal motion of the optical beam deflector for use in speckles removal subsequent to detection. Said super-imposed movements of the beam deflector are such that the beam exposes every point on the target equally (with the same amount of light) during acquisition time.

The method for speckles removal of the present invention reduces optical noise caused by retina (target) non-uniformity. Said super-imposed movements (A) move the illuminating zone over an area larger than that zone, (B) concurrently move the imaging zone so that the image of the illuminated zone does not move on the imaging device (even though it was scanned over a zone larger than the instantaneously illuminated and/or imaged zone), and (C) does this process in a time shorter than the image acquisition time.

The focus of the picture is very important. The operator adjusts the focus lens (9) to get as sharply focused a picture as is possible. The operator subjectively determines this from the definition of a slit image on the retinal tissue that the operator sees on the apparatus's computer monitor. Another option to achieve focus adjustment is to adjust the focus lens until the slit profile corresponding to the center of the area to be measured appears on the monitor at a preset point at which the slit appears when the system was calibrated.

The camera for imaging the pupil/iris produces an image of the eye being checked. The operator can observe the pupil and adjust the vertical and horizontal position for the apparatus in order to select a preferred section of the cornea through which the retinal measurement is to be executed. This image is focused by the operator by adjusting the distance between the apparatus and the patient's eye. The F number of this camera's lens is small and therefore the depth of field of the focus is small. Once the image is sharp, the distance from the system to the patient's iris is always the same as when adjusted while calibrating the system.

Figure 4 represents a schematic graph of beam position in the eye versus time. The time axis is divided into windows of image acquisition (23) and non-imaging windows (24). The beam position in the eye during the image acquisition window remains fixed with oscillation imposed, such that every point on the target is equally exposed. During the non-imaging window the position of the beam is moved to its next location.

Assume that every frame (every 40 msec) the image from the CCD is stored. This image is called a slit image. During the CCD Vertical Fly Back time, the beam deflector jumps to the next location which is shifted 200μ on the retina. This

process is repeated 10 times so that the slit images cover an area 2 mm wide.

In order to operate the Speckle Remover, the beam deflector is vibrated while an image is being acquired. The vibration amplitude on the retina is larger than the speckle or the non-uniformity size, for example 70 μ . The vibration can be composed of an integer number of back and forth movements during this time. The image on the CCD is not blurred due to this movement since it images the retina thru the same beam deflector that moves the laser beam on the retina.

Still the optic signal collected is from the whole area that was illuminated by the laser during the operation of the speckle remover. Since area (25a) is equal to area (25b), the camera receives a homogeneous blur of the speckle remover zone.

The present invention also relates to a method for imaging the eye and its components using the apparatus as defined, comprising;

(a) simultaneously using three optical paths for scanning the retina using a common optical beam deflector or deflectors to illuminate a predetermined zone of the retina and to acquire an image of said zone, while vibrating said beam deflector during said illumination/acquisition time, and said vibrations improve the image quality; imaging the whole Fundus; and imaging of the pupil/iris;

(b) subsequently spatially integrating one or more of said imagings into an eye model.

In the method according to the present invention the eye model may be represented in a format for retinal thickness mapping data (a) visualized as iso-thickness countour lines, (b) with a false coloration scale imposed in a thickness relevant fashion, (c) graphed onto various coordinate systems, for visualization of potential causal correlations, (d) for comparative transformations with previous imagery for the same area of the eye for the same patient, or according to demographic, genetic, physiological, or other factors, or (e) for quantitative evaluation, patient treatment, and comparison with previous or future results.

CLAIMS

1. A three dimensional imaging scanning apparatus for retinal thickness and structure non-invasive analysis comprising at least one optical path having a high brightness light source or a laser providing a beam for illuminating a selected portion of the retinal tissue; means for simultaneous focusing said beam going to the retina and returning from the retina wherein the said focusing means are common for both the beam going to and coming from the retina; an optical beam deflector common for both the beam going to and coming from the retina; an aperture for defining the angle between the beam going to the retina and returning from the retina; and detection means for detection of the returned beams and for determination of the retinal thickness.
2. Apparatus according to claim 1 having a second optical path with a light source illuminating the eye and the reflected light is sensed by an iris camera.
3. Apparatus according to claims 1 and 2 wherein a fundus illuminating light source illuminates the fundus and the reflected light is sensed by a camera.
4. Apparatus according to claim 3 wherein the fundus illuminating light source is a halogen lamp.
5. Apparatus according to claim 1 wherein the light source is from any type of coherent monochromatic laser, a bright diode, or an arc lamp.
6. Apparatus according to claim 5 wherein the light source provides or can be filtered to provide approximately green, yellow, or orange light.

7. Apparatus according to claim 1 having a beam shaping unit for insuring appropriate width and height of the beam on the fundus.

8. Apparatus according to claim 1 having at least one attenuator in the laser beam path for limiting the intensity of the light exposure to the retina.

9. Apparatus according to claim 1 wherein the detection means are a CCD camera.

10. Apparatus according to claim 1 wherein super-imposed movements of predetermined amplitude are super-imposed onto the motion of the optical beam deflector for use in speckles removal subsequent to detection.

11. Apparatus according to claim 10 wherein the super-imposed movement of the beam deflector causes the beam to expose every point on the target area equally during acquisition time.

12 A method for speckles removal for use in the apparatus according to the preceding claims for reducing optical noise caused by retina non-uniformity wherein said super-imposed movements move the illuminating zone on the retina over an area larger than that zone, concurrently moving the imaging zone so that the image of the illuminated zone does not move on the imaging device, and the superimposed movements are done in a time shorter than the image acquisition time.

13. A method for imaging the eye and its components using the apparatus as defined in the proceeding claims, comprising;

(a) simultaneously using three optical paths for scanning the retina using a common optical beam deflector or deflectors to illuminate a predetermined zone of the retina and to acquire an image of said zone, while vibrating said beam deflector during said illumination/acquisition time, and said vibrations improve the image quality; imaging the whole Fundus; and imaging of the pupil/iris;

(b) subsequently spatially integrating one or more of said imagings into an eye model.

14. A method according to claim 13 wherein the eye model is represented in a format for retinal thickness mapping data visualized as iso-thickness countour lines.

15. A method according to claim 13 wherein the eye model is represented in a format for retinal thickness mapping data with a false coloration scale imposed in a thickness relevant fashion.

16. A method according to claim 13 wherein the eye model is represented in a format for retinal thickness mapping data graphed onto various coordinate systems, for visualization of potential causal correlations.

17. A method according to claim 13 wherein the eye model is represented in a format for comparative transformations with previous imagery for the same area of the eye for the same patient, or according to demographic, genetic, physiological, or other factors.

18. A method according to claim 13 wherein the eye model is represented in a format for quantitative evaluation, patient treatment, and comparison with previous or future results.

1/3

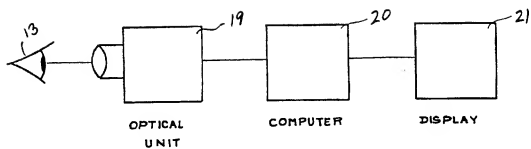


FIG 1

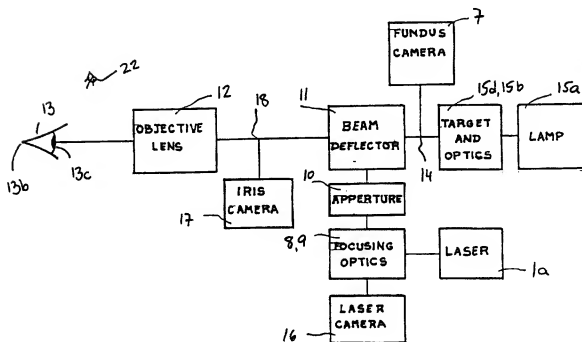
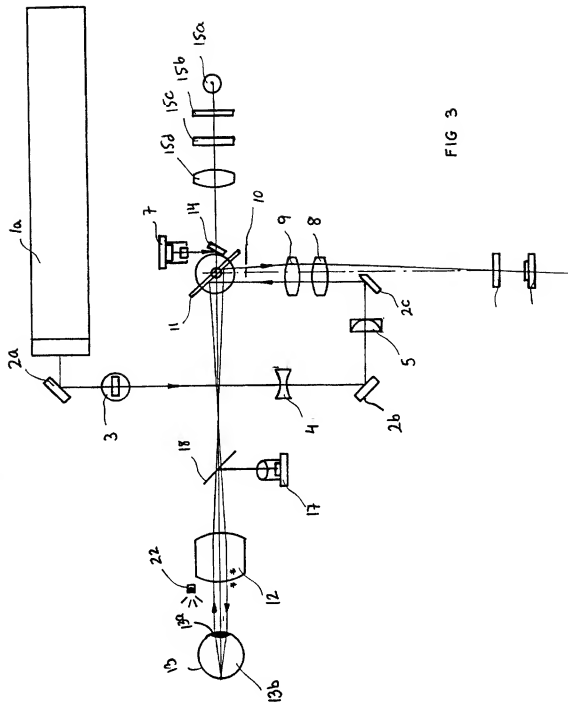
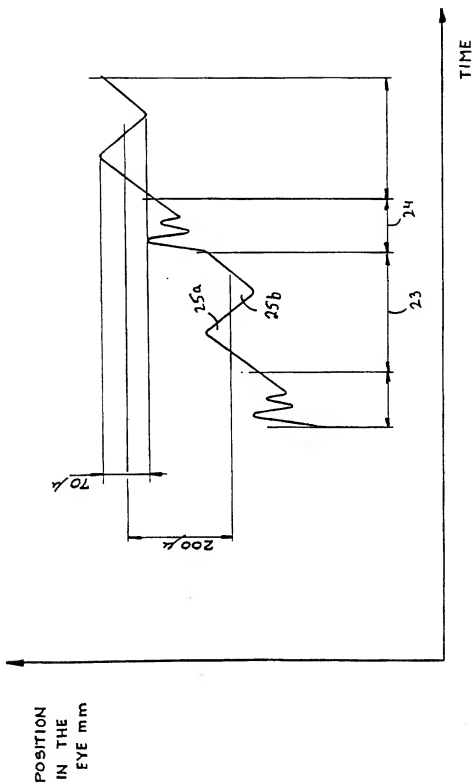


FIG 2





INTERNATIONAL SEARCH REPORT

International application No.
PCT/IL97/00065**A. CLASSIFICATION OF SUBJECT MATTER**

IPC(6) : A61B 3/14, 3/10, 3/00

US CL : 351/205, 206, 209, 210, 211, 214, 221, 246; 396/18

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 351/205, 206, 209, 210, 211, 214, 221, 246; 396/18

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

APS

search term: fundus, retina, scanning, shaping, focussing, deflect, thickness

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5,303,709 A (DREHER ET AL) 19 April 1994 (19.04.94), see entire document.	1-18
X, P	US 5,537,162 A (HELLMUTH ET AL) 16 JULY 1996 (16.07.96), see entire document.	1-18
X	US 4,991,953 A (PFLIBSEN ET AL) 12 FEBRUARY 1991 (12.02.91), see entire document.	1-18
X	US 4,569,354 A (SHAPIRO ET AL) 11 FEBRUARY 1986 (11.02.86), see entire document.	1-18

☒ Further documents are listed in the continuation of Box C.☐ See patent family annex.

* Special categories of cited documents:

A document defining the general state of the art which is not considered to be of particular relevance

E earlier document published on or after the international filing date

L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

O document referring to an oral disclosure, use, exhibition or other means

P document published prior to the international filing date but later than the priority date claimed

**

later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

X

document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

Y

document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

A

document member of the same patent family

Date of the actual completion of the international search

16 JUNE 1997

Date of mailing of the international search report

27 JUN 1997

Name and mailing address of the ISA/US
Commissioner of Patents and Trademarks
Box PCT
Washington, D.C. 20231

Facsimile No. N/A

Authorized officer

HUY MAI *Huy Mai*

Telephone No. (703) 308-4874